

# Damping

$\Delta > 0$  overdamped  $\delta > 1$   
 $\Delta < 0$  underdamped  $\delta < 1$   
 $\Delta = 0$  critically damped  $\delta = 0$

$\Delta = b^2 - 4ac$   
 $s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$   
 $\zeta =$  type of damping  
 $\omega_n =$  angular frequency  
 $\zeta =$  damping coefficient

$\ddot{x} + 2\zeta\omega_n \dot{x} + \omega_n^2 x = F$

Characteristic EQ:  $s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$

$x(t) = k_1 e^{s_1 t} + k_2 e^{s_2 t} + x(t \rightarrow \infty)$   
 $s = -\zeta\omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$

$V_L(t)$  should always lead  $I_L(t)$   
 $V_C(t)$  will always lag  $I_C(t)$  by  $90^\circ$   
 $i(t) = 5 \sin(420t + 20^\circ)A$   $v(t) = 10 \cos(420t + 70^\circ)$   
 $-20^\circ + 90^\circ = 70^\circ$  leads  $V$  by  $40^\circ$

$v_C(t) = (v_C(0^-) - v_C(t \rightarrow \infty))e^{-t/\tau} + v_C(t \rightarrow \infty)$   
 $v_C(0^-) = v_C(0^+)$   
 $i_L(0^-) = i_L(0^+)$   
 Continuity condition

# Max Power Transfer

$i(t) = |I| \cos(\omega t)$   
 $I_{rms} = \frac{|I|}{\sqrt{2}}$   
 $P_{avg} = \frac{1}{2} |I|^2 R \rightarrow I_{rms}^2 R(\omega)$

$Z_C = \frac{1}{j\omega C}$   
 $Z_L = Lj\omega$   
 $Z_R = R$

Find impedance of Load?  
 Test source method  
 • turn off all sources  
 • input test  $\oplus$  over load  
 $Z_{in} = \frac{V_T}{I_T} = V_{impedance}$

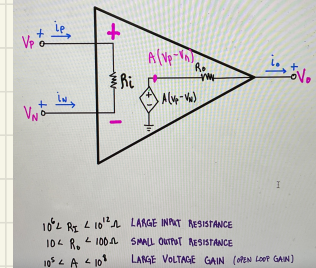
# IDEAL OP-AMP

$R_i \rightarrow \infty$   $R_o \rightarrow 0$   $A \rightarrow \infty$   
 $I_o = I_{in} = 0$   
 $\hookrightarrow \frac{V_o}{V_s} = -\frac{R_F}{R_s}$

$\omega = 2\pi f$   
 $v(t) = V_A \cos(\omega t + \phi)$   
 $V_A = \sqrt{a^2 + b^2}$   $a = V_A \cos(\phi)$   $b = V_A \sin(\phi)$   
 $\phi = \tan^{-1}(\frac{b}{a})$   
 $\underline{a}$  and  $\underline{b} \Rightarrow \underline{A} \cos(\omega t) + \underline{B} \sin(\omega t)$

$\omega_c = \frac{1}{L}$  for inductors  
 $= \frac{1}{\sqrt{LC}}$  for LC circuits  
 $\omega_c = \frac{1}{C}$

Inductor in series high pass filter  
 Capacitor in series low pass filter



# QUALITY FACTOR Qo

QUALITY FACTOR is the degree of selectivity of the circuit  
 HIGH Q  $\rightarrow$  NARROW BANDWIDTH & HIGH SELECTIVITY

$Q_o \equiv \frac{\omega_o}{\Delta\omega}$  (NARROW BANDWIDTH)  
 $Q_o = \frac{1}{2\zeta}$  (DAMPING RATIO)  
 OVERDAMPED  $Q_o < \frac{1}{2}$   $\zeta > 1$   
 UNDERDAMPED  $Q_o > \frac{1}{2}$   $\zeta < 1$   
 CRITICALLY DAMPED  $Q_o = \frac{1}{2}$   $\zeta = 1$

# TRANSFER FUNCTION

$H(j\omega) = \frac{V_{out}(j\omega)}{V_{in}(j\omega)}$  VOLTAGE GAIN TRANSFER FUNCTION  
 $|H(j\omega)| = \frac{\sqrt{a^2 + b^2}}{\sqrt{c^2 + d^2}}$  MAGNITUDE  
 $\angle H(j\omega) = \tan^{-1}(\frac{b}{a}) - \tan^{-1}(\frac{d}{c})$  PHASE (degrees)  
 CONVERT FROM dB TO VOLTS  $\#V = 10^{\frac{\#dB}{20}}$

$P(j\omega) = H^2(j\omega)$   
 $P(j\omega_c) = \frac{H_o^2}{2}$   
 "-3dB" half power

### Problem 2 - Frequency Response, Magnitude

a) [2.5pts]  $V_C(j\omega)$  is resonant at  $10\text{krad/s}$  with  $|V_C(j\omega_0)| = 0.5V$  determine the numerical value of C in Farads.

$V_C(j\omega) = I_s(j\omega)Z_C \rightarrow -\frac{j}{\omega C}(\frac{1}{2})(1+j) = \frac{-1-j}{2(\omega C)}$   
 $|V_C(j\omega)|_{\omega=\omega_0} = 0.5 = \frac{\sqrt{2}}{2(10\text{krad/s})C}$   
 $C = \frac{1}{0.5 \times 10^4} = 141\mu F$

b) [2.5pts] By hand, sketch  $|V_C(j\omega)|_V$

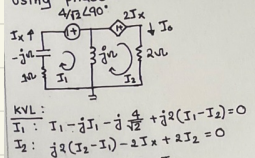
$|V_C(\frac{j\omega_0}{100})|_{\omega < \omega_0} = \frac{1}{\frac{10^4}{100}(200\mu F)} \rightarrow 0.5V$   
 $|V_C(j\omega_0)|_{\omega = \omega_0} = \frac{1}{10^4(200\mu F)} \rightarrow 0.5V$   
 $|V_C(j100\omega_0)|_{\omega > \omega_0} = \frac{1}{10^4(200\mu F)} \rightarrow 0.005V$

### Problem 3 - Saturation

a) Derive an expression for the Dynamic Linear Range of the output voltage in terms of  $\pm V_{CC}$ ,  $V_{sat}$ , and the resistor. Recall  $-V_{CC} < V_o < V_{CC}$

LINEAR RANGE of operation for OPAmp  
 $-15V \leq (\frac{V_o}{10})(V_{sat} + 1) \leq 15V$   
 $-10V \leq 5V_{sat} + 5 \leq 15V$   
 $-20V \leq 5V_{sat} \leq 10V$   
 $-4V \leq V_{sat} \leq 2V$

### Mesh with dependent source



Using phasors  $4\sqrt{2} \angle 90^\circ$

KVL:  $I_1 - jI_2 - j \frac{4}{\sqrt{2}} + jI_2(I_1 - I_2) = 0$

$I_1: I_1 - jI_2 - j \frac{4}{\sqrt{2}} + jI_2(I_1 - I_2) = 0$

$I_2: jI_2(I_1 - I_2) - 2I_1 + 2I_2 = 0$

AUX:  $I_1 = I_x \quad I_2 = I_o$

After solving the 2 eqn:

$(1-j)I_o = j \frac{4}{\sqrt{2}}$

$I_o = j \frac{4}{\sqrt{2}(1-j)} \times \frac{(1+j)}{(1+j)}$

$= j \frac{4}{\sqrt{2}} \frac{(1+j)}{(1-j)}$

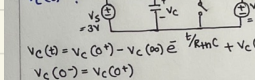
$= \frac{2}{\sqrt{2}}(j-1)$

$|I_o| = \frac{2}{\sqrt{2}} \times \sqrt{2} = 2$

$\angle I_o = 135^\circ [90 + 45]$

$I_o(t) = 2 \cos(\omega t + 135)$

### Transient Response



$V_c(t) = ?$

$V_c(t) = V_c(\infty) - v_c(\infty) e^{-t/\tau} + V_c(0)$

At DC  $V_c(0) = ?$

$V_c(\infty) = V_c(\infty) - v_c(\infty) e^{-t/\tau} + V_c(0)$

$V_c(0) = 3V$

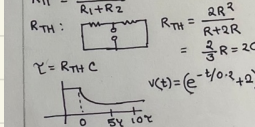
$V_c(\infty) = 3V \left( \frac{3R}{R+3R} \right) = 2V$

$R_{TH} = \frac{R_1 R_2}{R_1 + R_2} = \frac{3R \cdot 3R}{3R + 3R} = \frac{9R}{6} = \frac{3R}{2}$

$R_{TH} = \frac{3R \cdot 3R}{R+3R} = \frac{9R}{4}$

$\tau = R_{TH} C = \frac{3R}{2} C$

$V_c(t) = (e^{-t/(\frac{3R}{2}C)} + 2)V$



Dynamic Opamp

$A: \left( \frac{1}{R_1} + \frac{1}{R_2} + j\omega C_1 \right) A - \frac{V_p}{R_1} - \frac{V_p}{R_2} - V_o j\omega C_1 = 0$

$V_p: \left( \frac{1}{R_3} + j\omega C_1 \right) V_p - \frac{V_o}{R_2} = 0$

$V_n = V_p = V_o$

↳ negative feedback

$\frac{V_o}{V_s} = H(j\omega)$

### NOTE

RLC standard form:  $s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$

$\omega_n = \sqrt{1/LC} = \frac{1}{\sqrt{LC}}$

\* voltage leads - inductor

current leads - capacitor.

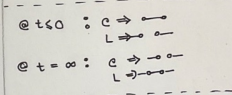
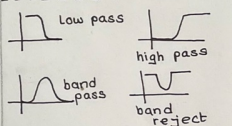
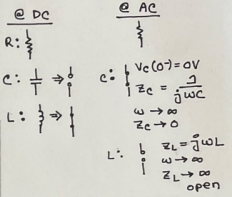
Resonance,  $\omega_0$

$X_L = X_C$

$j\omega_0 L = \frac{j}{\omega_0 C}$

$\omega_0^2 = \frac{1}{LC}, \omega_0 = \frac{1}{\sqrt{LC}}$

$dB_V = 20 \log_{10} |H(j\omega)|$



### 1st order

For capacitor:  $V_c(t) = [V_c(0) - V_c(t \rightarrow \infty)] e^{-t/\tau} + V_c(t \rightarrow \infty)$

$\tau = R_{TH} C$

For inductor:  $i_L(t) = [i_L(0) - i_L(t \rightarrow \infty)] e^{-t/\tau} + i_L(t \rightarrow \infty)$

$\tau = \frac{L}{R_{TH}}$

